

LRFD

Section 3.75

New: January 2005

CLICK HERE TO Index

Concrete Semi-Deep Abutments - Section 3.75

Index

Page: i-1

3.75.1 General

1.1 Material Properties

3.75.2 **Design**

- 2.1 Limit States and Factors
- 2.2 Distribution of Loads
- 2.3 Design Assumptions
- 2.4 Design Process

3.75.3 Geometry

- 3.1 Wing Elevation
- 3.2 Cross-Section
- 3.3 Plan View
- 3.4 Front Elevations
- 3.5 Pile Location

3.75.4 Reinforcement

- 4.1 Front Elevation
- 4.2 Wing Elevation
- 4.3 Cross-Section
- 4.4 Plan View
- 4.5 Bearing Beam
- 4.6 Pile Haunches

3.75.5 **Details**

- 5.1 Front Sheet
- 5.2 Ground line within Abutments
- 5.3 Construction Joints
- 5.4 Access Door

LRFD Bridge Design Guidelines

Concrete Semi-Deep Abutments - Section 3.75

General

Page: 1.1-1

3.75.1 General

1.1 Material Properties

Concrete

Class B Concrete (Substructure

$$f'_c = 3.0 \text{ ksi}$$

 $n = 10 \text{ ksi}$

Class B-2 Concrete (Abutment Slab)

$$f'_c = 4.0 \text{ ksi}$$

 $n = 8 \text{ ksi}$

LRFD 5.4.2.4 Concrete modulus of elasticity,

$$E_c = 33000 K_1 w_c^{1.5} \sqrt{f'_c}$$

Where:

 w_c = unit weight of non-reinforced concrete = 0.145 kcf K_1 = correction factor for source of aggregate = 1.0

LRFD 5.4.2.6

Modulus of rupture: For minimum reinforcement,

$$f_r = 0.37 \sqrt{f'_c}$$

For all other calculations,

$$f_r = 0.24 \sqrt{f'_c}$$

$$\sqrt{f^{\, \prime}_{\ c}}^{\, }$$
 is in units of ksi

Reinforcing Steel

LRFD 5.4.3.1 Minimum yield strength, *LRFD 5.4.3.2* Steel modulus of elasticity, $f_{y} = 60.0 \text{ ksi}$

 $E_{\rm S} = 29000 \, \rm ksi$

Piling

See LRFD DG Sec. 3.80 for pile capacity. Also check the Design Layout sheet if a pile capacity is indicated.

Concrete Semi-Deep Abutments - Section 3.75

Design

Page: 2.1-1

3.75.2 <u>Design</u>

2.1 Limit States and Factors

In general, each component shall satisfy the following equation:

LRFD 1.3.2.1

$$Q = \sum \eta_i \gamma_i Q_i \le \phi R_n = R_r$$

Where:

Q = Total factored force effect

 Q_i = Force effect

 $\eta_i = \text{Load modifier}$

 γ_i = Load factor

 ϕ = Resistance factor R_n = Nominal resistance R_r = Factored resistance

LRFD 5.5

Limit States

The following limit states shall be considered for abutment design:

STRENGTH - I

STRENGTH – III

STRENGTH – IV

STRENGTH - V

SERVICE – I

FATIGUE

EXTREME EVENT - II

See LRFD Table 3.4.1-1 and LRFD 3.4.2 for Loads and Load Factors applied at each given limit state.

Resistance factors

LRFD 6.5.4.2 STRENGTH limit states, see LRFD 6.5.4.2 and LRFD 5.5.4.2

LRFD 1.3.2.1 For all other limit states, $\phi = 1.00$

LRFD 1.3.2.1 Load Modifiers

For loads where a maximum value of load factor is appropriate:

 $\eta = (\eta_I \eta_R \eta_D) \ge 0.95$

For loads where a minimum value of load factor is appropriate:

 $\eta = 1 / (\eta_I \eta_R \eta_D) \le 1.0$

Where:

LRFD 1.3.3 η_D = Factor relating to ductility LRFD 1.3.4 η_R = Factor relating to redundancy

LRFD 1.3.5 η_i = Factor relating to operational importance

LRFD Bridge Design Guidelines

Concrete Semi-Deep Abutments – Section 3.75

Design

Page: 2.1-2

Table 3.75.2.1 Load modifiers

	All Limit States			
Ductility, η_D	1.0			
Redundancy, η_R	1.0			
Operational importance, η_I	1.0			
$\eta = (\eta_I \ \eta_R \ \eta_D)$	1.0			
$\eta = 1 / (\eta_I \eta_R \eta_D)$	1.0			

Design

Page: 2.2-1

2.2 Distribution of Loads

Dead Loads

Loads from stringers/girders shall be applied as concentrated loads at the intersection of the centerline of stringer/girder and the centerline of the bearing.

Loads from Abutment components (Abutment Slab, Barrier Curb, Wings, Apron, Curtain Wall, etc) shall be applied to the Bearing Beam and Transverse Approach Beam respectively as uniform distributed loads for the computation of pile loads and reinforcement.

Live Loads

Loads from stringers/girders shall be applied as concentrated loads at the intersection of the centerline of stringer/girder and the centerline of the bearing.

Loads from the Abutment Slab shall be applied to the Transverse Approach Beam as a uniform distributed load for the computation of pile loads and reinforcement. No Live load shall be distributed through the Abutment Slab to the Bearing Beam for computations of pile loads or reinforcement

Wind, Temperature, Frictional Loads

These loads shall be disregarded, except for special cases or if specified by the Structural Project Manager, or on the Design Layout Sheet.

Earth Pressure Loads

Earth pressure loads are applied to the apron wall and part of the wing wall that extends past the transverse approach beam respectively. All tables have these forces already incorporated. For all special designs, these forces shall be applied appropriately.

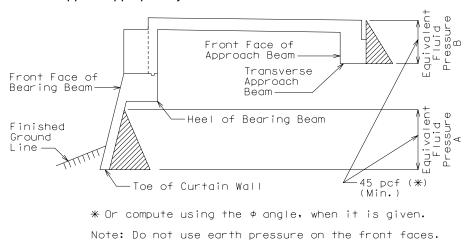


Figure 3.75.2.2.1 Elevation

Design

Page: 2.3-1

2.3 Design Assumptions

Abutment Slab

Assume a uniform 3" wearing surface load.

Assume slab to be acting one-way parallel with roadway.

Bearing Beam

The beam is assumed continuous over supports at centerline of piles.

Live loads are applied to the superstructure only. Live loads are not simultaneously applied to the abutment slab.

Transverse Approach Beam

The beam is assumed continuous over supports at centerline of piles.

The beam is assumed to carry half of the dead load of the approach slab.

Live loads are applied to the abutment slab only. Live loads are not simultaneously applied to the approach slab.

Apron Wall

Assume apron wall to be cantilevered off of bearing beam with no support from battered piles.

Use an equivalent fluid pressure of 45 pcf.

Wing Wall

Assume wing wall to be cantilevered at the fill face side of the transverse approach beam.

Assume 1'-0" of soil braces wing wall bottom at short end of wall.

Use an equivalent fluid pressure of 45 pcf.

Include a collision impact load applied to the barrier curb transferred to the wing.

Assume LL surcharge lateral load of 90 pcf.

Piles

Stresses in the piles due to bending need not be considered in design calculations, except for seismic design.

LRFD Bridge Design Guidelines

Concrete Semi-Deep Abutments - Section 3.75

Design

Page: 2.4-1

2.4 Design Process

There are many ways to go about designing a Semi-Deep Abutment. Below is one process, which will work for most standard abutments. A majority of the steps are interchangeable, and can be switched to meet the designers' preference.

Design geometry of abutment

Calculate the size and number of piles required for the bearing beam

Determine the bearing beam reinforcement

Calculate the size and number of piles required for the transverse beam

Determine the other abutment components reinforcement

<u>G</u>eometry

Page: 3.1-1

3.75.3 Geometry

Use the standard illustrations in this section, information from your superstructure calculations, and the design layout sheet to design the geometry of the abutment.

3.1 Wing Elevation

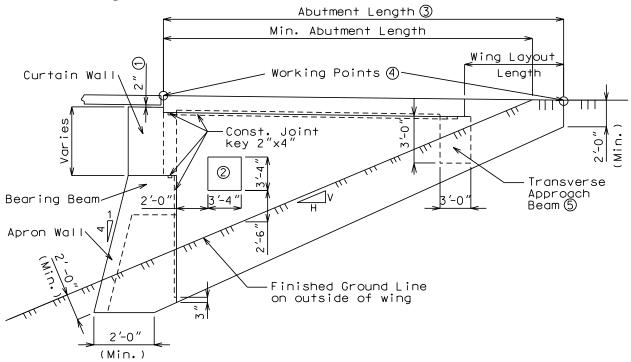


Figure 3.75.3.1 Wing Elevation

- ① Top of curtain wall to be 2" below the slab of the adjoining span.
- ② An access door shall be used only when called for on the Design Layout Sheet.
- It may be necessary to increase Abutment Length so end of wing extends beyond the intersection of the ground line and top of slab at the outside edge of wing.
- 4 Working points shall include elevations at grade for the bridge.
- Slope Transverse Beam both top and bottom when the Abutment Slab haunch exceeds 6" (at gutter line).

Page: 3.2-1

Geometry

3.2 Cross-Section

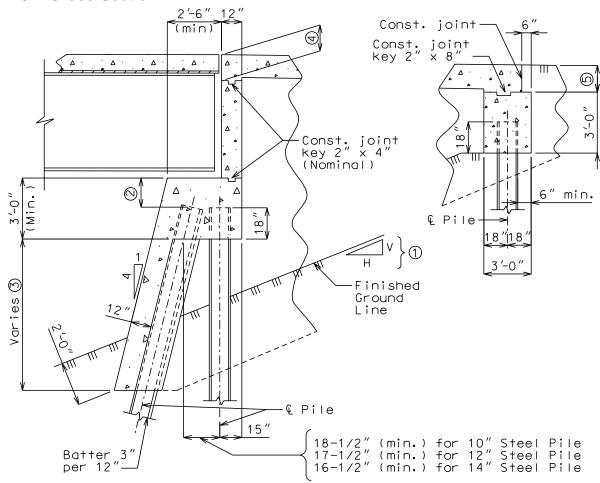
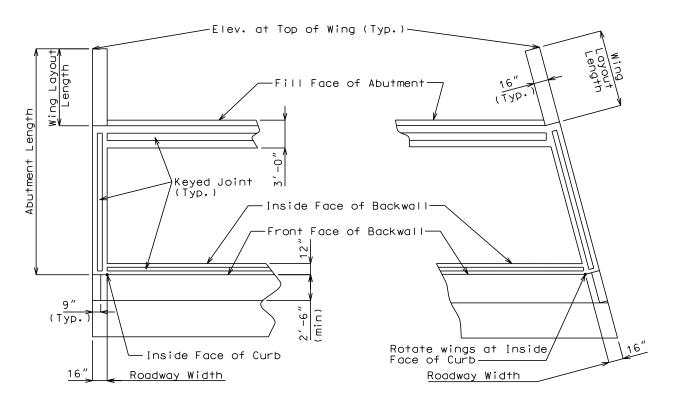


Figure 3.75.3.2 Cross-Section

- 1 Check the profile sheet with Design Layout for the slope of finish ground line.
- 2 Check the clearance of anchor bolt wells; increase beam depth if needed.
- 3 If length is greater than 15'-0", Apron wall reinforcement shall be designed.
- 4 Abutment Slab Depth + ½" (min.)
- (5) 12" (min.) at gutter line to the top of the Transverse Approach Beam, except when the Abutment Slab depth is 12" or greater, then place the top of the Transverse Approach Beam ½" below the bottom of the slab.

Page: 3.3-1
Geometry

3.3 Plan View



Square Structures

Skewed Structures

Figure 3.75.3.3 Plan View

Page: 3.4-1
Geometry

3.4 Front Elevation

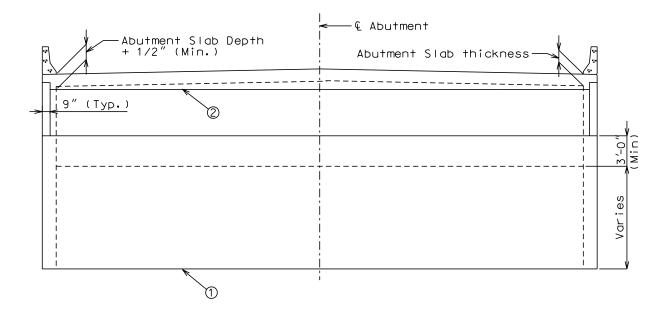


Figure 3.75.3.4 Front Elevation

- ① Slope toe of Apron Wall when the ends of the walls differ in elevations by more than 2'-0". (or when beam is sloped)
- ② Slope top of backwall when the slab haunch exceeds 6" (at gutter line).

Geometry

Page: 3.5-1

3.5 Pile Location

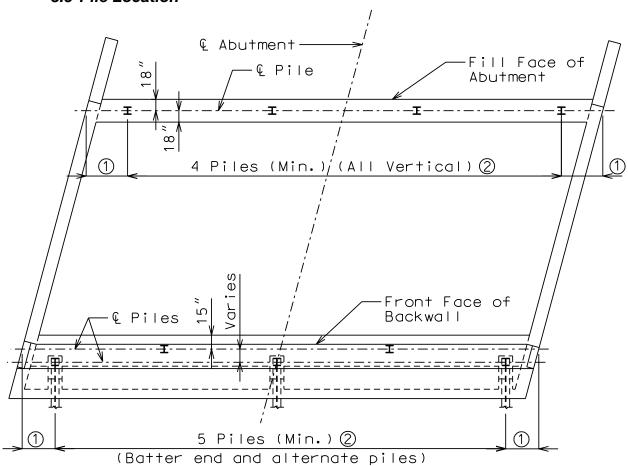


Figure 3.75.3.5 Pile Location

- ① 21" (Min.), 2'-0" (Max)
- ② 30" or 2.5 X pile diameter (Min.), 12'-0" (Max.) spacing, 1" increments

Page: 4.1-1

Reinforcement

3.75.4 Reinforcement

4.1 Front Elevation

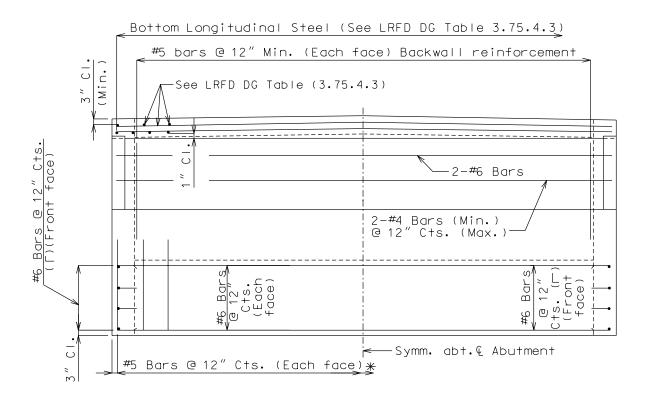


Figure 3.75.4.1 Front Elevation

All transverse steel to be placed parallel to the backwall. All main steel to be placed parallel to the centerline of roadway

Epoxy coat all reinforcing in abutment slab, bearing beam, curtain wall, apron wall, backwall, and transverse approach beam.

See LRFD DG Sec. 3.35 for details of protective coating and sloping top of beam to drain.

* If height of Equivalent Fluid Pressure A (LRFD DG Figure 3.75.2.2) is greater than 5 ft. or if apron wall extends more than 15 ft. below bearing beam, reinforcement will need to be verified.

Page: 4.2-1

Reinforcement

4.2 Wing Elevation

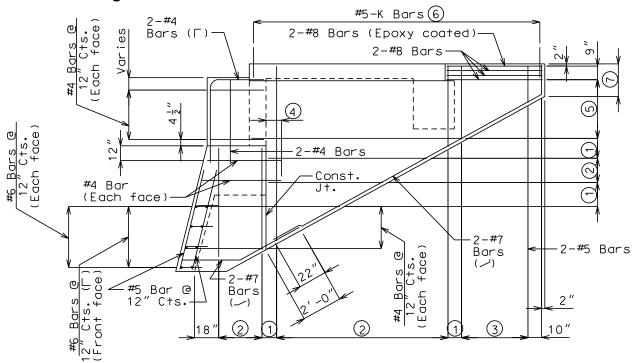


Figure 3.75.4.2 Wing Elevation

- ① Varies (12" Max.)
- 2 #4 Bars at 12" cts. (Each face)
- 3 #5 Bars at 12" cts. (Each face)
- ④ 12" (Min.) (Development length)
- ⑤ #6 Bars at 8" cts. (Each face)
- © See LRFD DG Sec. 3.32 for barrier curb details and spacing of K bars.
- If end of wing wall is greater than 5'-0" deep, reinforcement will need to be verified.

Page: 4.3-1

4.3 Cross Section

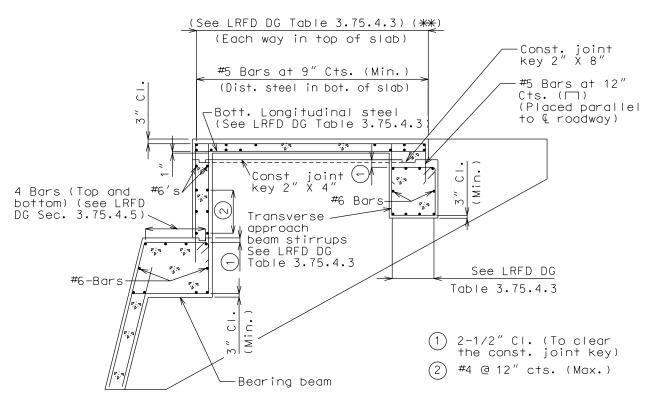


Figure 3.75.4.3 Cross Section

For notes, see page 4.3-2

LRFD Bridge Design Guidelines

Concrete Semi-Deep Abutments - Section 3.75

Reinforcement

Page: 4.3-2

Table 3.75.4.3 Reinforcement

Abutment Slab Design Lengths (*)	Uniform Axle Abutment Slab Thickness Axle Vehicle Live Load (***)	Abutment Slab Bottom Steel	Abutment Slab Top	Transverse Approach Beam Reinforcement (Top & Bot.) ****						
			Parallel to C.L. Rdwy.	Steel Each Way	Pile Spacing					
		()			<u><</u> 7'	8'	9'	10'	11'	12'
10'-0"	11"	40.00 k	#8 at 9" cts.	#4 at 18" cts.	4-#6	4-#6	4-#6	4-#6	4-#7	4-#8
15'-0"	12"	43.33 k	#8 at 8" cts.	#4 at 12" cts.	4-#6	4-#6	4-#6	4-#7	4-#7	4-#8
20'-0"	15"	45.00 k	#8 at 7" cts.	#4 at 12" cts.	4-#6	4-#6	4-#7	4-#7	4-#8	4-#8
25'-0"	17"	46.08 k	#8 at 5" cts.	#4 at 12" cts.	4-#6	4-#6	4-#7	4-#7	4-#8	6-#8
30'-0"	20"	49.60 k	#9 at 6" cts.	#5 at 12" cts.	4-#6	4-#7	4-#7	4-#8	6-#8	6-#8
35'-0"	22"	52.80 k	#9 at 5" cts.	#5 at 12" cts.	4-#6	4-#7	4-#8	4-#8	6-#8	6-#8
Transverse Approach Beam Stirrup Size				#4	#4	#5	#5	#6	#6	

^{*} Abutment slab design length is measured from the center of the backwall to the center of the approach beam along the centerline of roadway.

^{**} For abutment slabs with lengths greater than 35'-0", an intermediate bent is required inside the semi-deep abutment. Top and bottom reinforcement for these slabs shall be designed by the designer.

^{***} Use the axle vehicle live load for calculating pile loads for the transverse approach beam.

^{**** 4-#9&#}x27;s can be used in lieu of 6-#8's if spacing restrictions require fewer bars.

Page: 4.4-1

4.4 Plan View

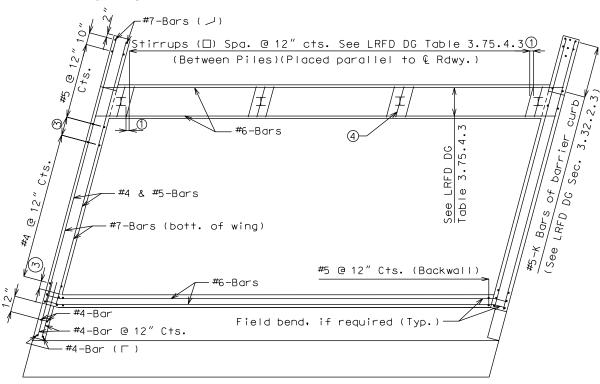


Figure 3.75.4.4.1 Section at Upper Construction Joint

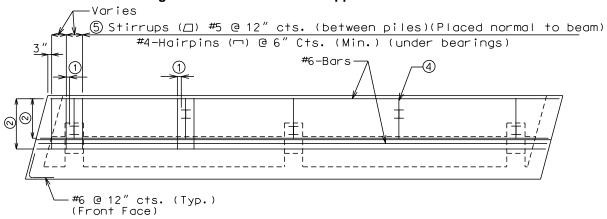


Figure 3.75.4.4.2 Plan of Bearing Beam below Lower Keyed Construction Joint

- ① Use 3" (min.) and 6" (max.) (Typ.)
- ② See LRFD DG Sec. 3.75.4.5
- ③ Varies (12" max.)
- Stirrup to be centered over pile (Typ.)
- ⑤ If nominal pile capacity is greater than 110 tons, stirrup size and spacing needs to be verified.

Page: 4.5-1
Reinforcement

4.5 Bearing Beam

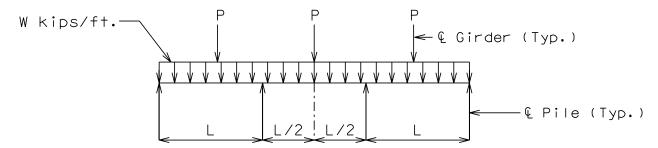


Figure 3.75.4.5.1 Basic Assumption (Continuous Beam)

$$M = 0.20PL + 0.13WL^2$$

 $P = Superstructure\ Loads\ (Applied\ through\ beam\ seat)$

 $W = Uniform \ DL \ (Abutment \ Components)$

 $L = Pile\ Spacing(ft.)$

$$M_u = 1.25 M_{DL} + 1.50 M_{FWS} + 1.75 M_{LL}$$

$$R_u = \frac{M_u}{\phi b d^2}$$

LRFD 5.5.4.2

$$\phi = 0.90$$

$$\rho = \frac{0.85 f'_{c}}{f_{y}} \left(1 - \sqrt{1 - \frac{2R_{u}}{0.85 f'_{c}}} \right)$$

LRFD 5.7.3.3

Max. Reinforcement
$$c/d_e \le 0.42$$

Min. Reinforcement
$$M_n > \min$$
.
$$\begin{cases} 1.2M_{cr} & \text{#6 Bars-} \\ 1.33M_u & \text{#6} \end{cases}$$

LRFD 5.7.3.4 Crack Control Parameters

$$\beta_s = 1 + \frac{d_c}{0.7(h - d_c)}$$

$$s \le \frac{700\gamma_e}{\beta_s f_s} - 2d_c$$

See LRFD DG Sec. 3.30.1.5

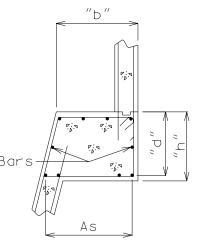


Figure 3.75.4.5.2

Page: 4.6-1

4.6 Pile Haunches

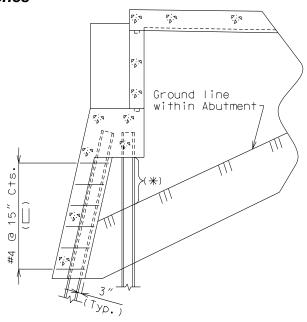


Figure 3.75.4.6.1 Part Section Thru Bearing Beam

(*) See LRFD DG Sec. 4.0 for appropriate notes for steel H pile and steel pile shells.

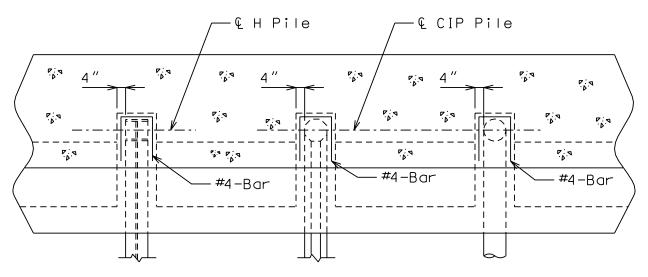


Figure 3.75.4.6.2 Plan of Bearing Beam below lower construction joint

(Showing typical dimensions for different pile types)

Page: 5.1-1

Details

3.75.5 Details

5.1 Front Sheet

Figure 3.75.5.1 is an example of the information to be included on the abutment plan view on the first sheet of the plans.

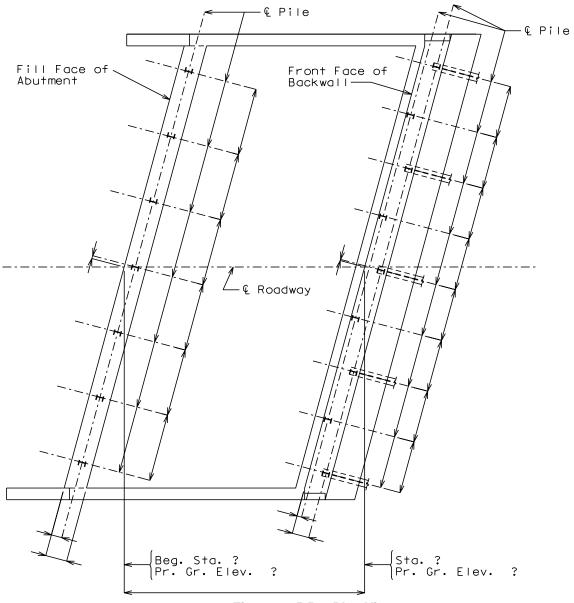


Figure 3.75.5.1 Plan View

Details for unsymmetrical roadways will require dimensions tying centerline of roadway to centerline of structure. (Pile coordinates shall be to centerline of roadway)

Details

Page: 5.2-1

5.2 Ground Line Within Abutments

Figure 3.75.5.2 shall be detailed on the first or second sheet of the plans.

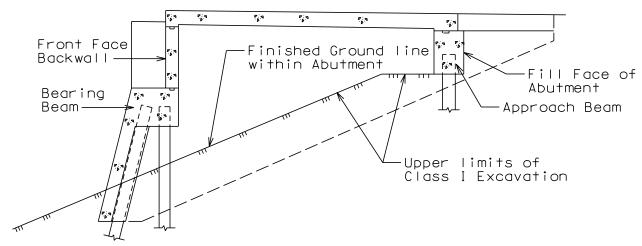


Figure 3.75.5.2 Ground Line and Piling in Abutments

Page: 5.3-1

Details

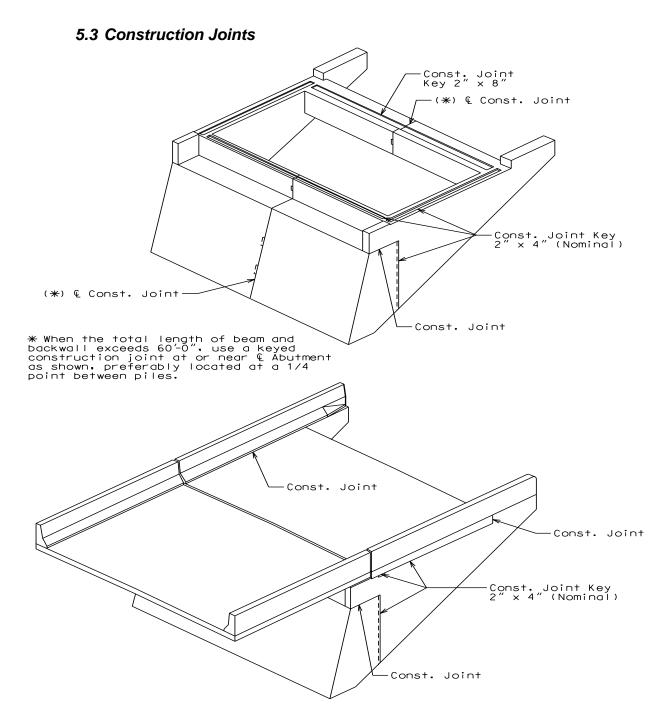


Figure 3.75.5.3 Construction Joints

Page: 5.4-1

Details

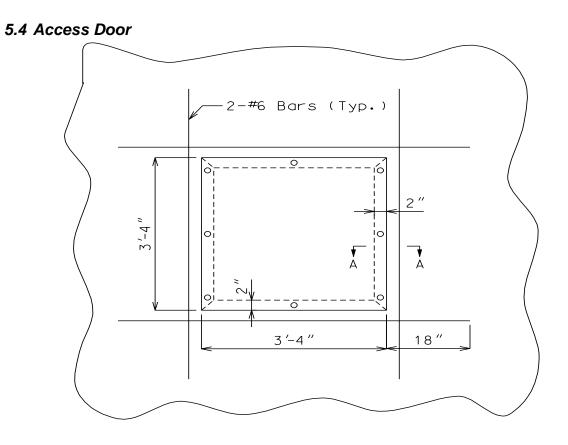


Figure 3.75.5.4.1 Door Elevation

Cost of the door is to be included in other items.

Cut or bend reinforcing steel in the field to clear the opening for the access door.

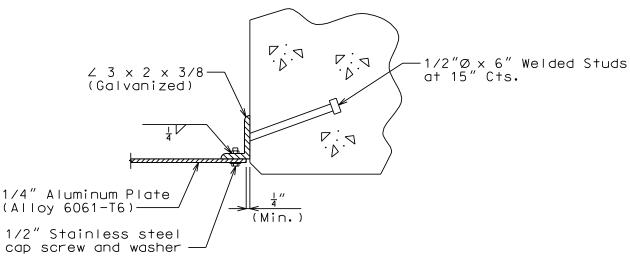


Figure 3.75.5.4.2 Section A-A